

# Finite Element Slope Stability Analysis By Geofoam Technique

Mahmoud S. El-kady, Essam Farouk, Wassef Ounaies, Muhammad Tariq Bashir

**Abstract:** Slope stability is one of the most important problems in geotechnical engineering because failure could cause catastrophic environmental and human disaster, in addition to large economical losses due to such failure. The simplest solution to handle with slope failures is to avoid the failed zones and choose safer locations to move the projects which are decided to be constructed nearby the failed slopes. The paper delineates the effects of geofoam on soft clayey slopes which contain weak layers. This emphasis is given to the slope geometry, loading, and geofoam material that are numerically simulated using the finite element technique. In addition, the proposed stabilizing system is employed, presented, and analyzed. The analysis of the embankment is performed by the limit equilibrium analysis program (Slide V6.003). The increase in the geofoam thickness from 0.0m to 1.0m resulted in a noticeable increase in the safety factor for loaded and unloaded slopes. On another hand, increase in geofoam thickness from 1.0m up to 4.0m in case of unloaded slope, the safety factor is still constant for about 2.10. A consistent increase in the safety factors is noticed as a result of increasing the geofoam thickness from 0.0m up to 4.0m. Moreover, there is a slight decrease in the safety factor for loaded slopes during different values of geofoam position from the road level. The main factors which affect the slopes stabilized with geofoam such as, geofoam width, thickness, and position of the geofoam from the road level are also presented and discussed.

**Index Terms:** Slope Stability, Geofoam, Local Failure, Slip Failure.

## 1 INTRODUCTION

Researchers were concerned in introducing techniques that help in evaluating and modeling slopes, in order to propose the correct judgment of the slope status, and choose the safe and economic technique to stabilize the endangered slopes [1]. There are different techniques used for stabilizing slopes and to increase the slope safety factor, such as rubble, and slope stabilizing piles. Slopes could fail under different types of external loads, changing in the surrounding environmental conditions such as the water table and many other reasons could cause such failures in the slope [1]. The slope must have a stabilizing system to increase the safety factor. The slope failures not only cause huge economical losses on the nearby projects, but also could cause human and environmental losses [2]. A main part in overcoming the slope failure problems is to identify the reasons which cause such problem. Subsequently, defining the cause(s) and gathering the required information about the slope, the geotechnical engineer judgment must intervene to choose the most suitable and economical stabilization system. The factor of safety (F.S.) for slope stability analysis is usually defined as the ratio of the ultimate shear strength divided by the mobilized shear stress at incipient failure. The most common formulation for F.S. assumes the factor of safety to be constant along the slip surface, and is defined with respect to the force or moment equilibrium [3]: Moment equilibrium: generally used for the analysis of rotational landslides. The F.S is defined with respect of moments.

Here,  $M_r$  and  $M_d$  stand for the sum of the resisting moments and sum of the driving moments, respectively. -Force equilibrium: generally applied to translational or rotational failures composed of planar or polygonal slip surfaces. The factor of safety (F.S.) in such case is defined with respect to force. Here,  $F_r$  and  $F_d$  refer the sum of the resisting forces and the sum of the driving forces, respectively. Thus, the slope safety factor could be computed from force and/or moment equilibrium equations. There are many reasons which could cause slope instability. The foremost reason that may lead to slope failure includes decreasing of the soil shear strength, existence of problematic soil layers within the slope soil profile such as; peat, collapsible or swelling soils, very soft clay...etc., externally applied high loads on the slope, and rapid drawdown of the water level in front of the slope, while the embankment slope itself is still fully saturated [4]. The different methods used for stabilizing slopes are divided mainly into three categories; either reducing the driving forces, or increasing the resisting forces, or both. There are large number of stabilizing systems which could be used in stabilizing slopes such as; accelerating the slope drainage rate which will consequently increase the soil shear strength, reducing the sliding mass weight by removing the upper part of the slope or the unstable part if possible depending on the location of this part, using light weight fill materials in slope construction, reducing the slope inclination angle, using retaining systems to support the slope, in addition to reinforcing the slope with piles (vertically), geosynthetics and geogrid (horizontally), nails (inclined)...etc[5]. Other stabilizing techniques are also possible such as dynamic compaction, jet grouting, slope vegetation, and chemical treatment for the slope to increase the shear strength parameters of the soil. Chemical treatment includes using lime or a mix of lime and cement columns and different in-situ soil mixing techniques. Opting the suitable system needed to be used in stabilizing a failed (or expected to fail) slope should be based mainly on identifying the main causes of slope failure, the expected circumstances which will affect the slope in the future, and the best economical solution [7].

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## 2 METHDOLOGY

The erosion or failure in slopes poses a great danger to nearby and surrounding communities. Such slope failure will cause great losses in life and property, and thus should be prevented by any means [8]. Thus, safety of such slopes is a major concern and should always be satisfied in working and extreme loading conditions. In this research the slope geometry, loading, and geofoam material are numerically simulated using the finite element technique. In addition, the proposed stabilizing system is employed, presented, and analyzed. The general configurations of the canal's slope are presented in Figure-1. The dimensions presented in the canal cross section, as shown in Figure-1, is based on data from several studies made on this slope starting with a general planning study performed by the Ministry of Irrigation, Egypt along with other studies like the one that performed by Al-Ashaal et al. (1998).

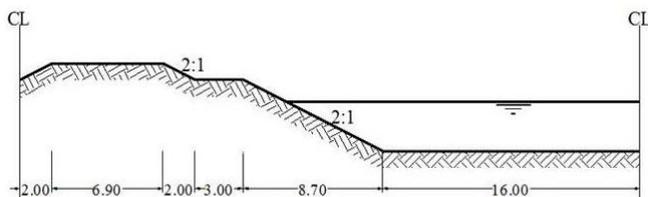


Fig. 1. Schematic Diagram of Canal Cross Section

The project of stabilizing and developing case of study of the Al-Salam canal contains two extensive monitoring zones from 8.800 km to 8.850 km and from 7.700 km to 7.750 km. These zones are mainly chosen due to the presence of the peat layer, as assured from the boreholes performed along the whole embankment length.

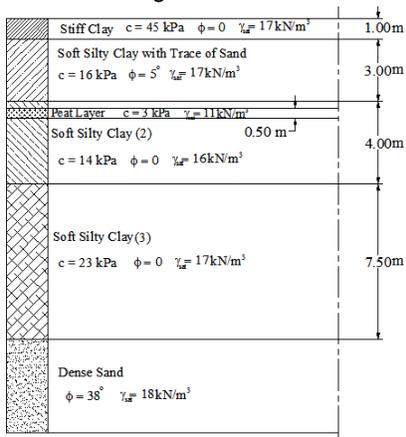


Fig. 2. The Slope Soil Stratification

## 3 MATERIAL PROPERTIES

Geofoam mechanical properties such compressive strength, elastic modulus, poisson's ratio, shear strength, flexural strength, stiffness, creep behavior and other mechanical properties depend on the Geofoam unit weight. It should be noted that the manufacturing cost of the Geofoam increases with the increase of the density. For practical civil applications, geofoam densities range between 11 and 30 kg/m<sup>3</sup> [5]. Geofoam densities are categorized by ASTM C 578-04 to 5 types, 12, 15, 18, 22, 29 kg/m<sup>3</sup>. The geofoam density used in

the research is 20 kg/m<sup>3</sup>. Higher values of geofoam densities are not used to minimize the actual cost. The properties of geofoam having a unit weight of 20 kg/m<sup>3</sup> manufactured in Egypt listed in Table (1).

TABLE 1. GEOFOAM BLOCK PROPERTIES. [12]

Geofoam properties	Value
Unconfined compressive strength at 10% strain, (kPa)	94.5
Initial elastic modulus, (kPa)	3549
Poisson's ratio	0.01
Angle of friction, (o)	15.87
Cohesion, (kPa)	27.07
Flexural Strength, (kPa)	245.4
Flexural Strain, (%)	6.3
The coefficient of compressibility, (MPa-1)	0.479
Compression Index	56.5
Recompression Index	2.51
Water absorption after 28 days, (%)	2.45%

## 4 THE FINITE ELEMENT PROGRAM DESCRIPTION

In the last decades, there were huge jumps in the field of computer science either in the software or in the hardware. The finite element analysis has proved to be a powerful tool in analyzing a wide range of geotechnical problems. Different algorithms were created and adapted in order to optimize the finite element solutions and reduce the time required for problem analysis. Applying the finite element method in geotechnical engineering allows for modeling many applications such as slope stability analysis, earth dams, tunnels, along with many dynamic applications. This powerful and flexible technique has the ability of simulating varies soil applications and conditions. In the current analysis, the different factors affecting the slope stability are taken into consideration to ensure the accuracy of the slope analysis results and specifying the important parameters that affect slopes; the soil shear strength parameters, the presence and the position of the peat layer within the slope, the slope inclination angle, the slope height, the external loads value, and the soil Young's modulus [4]. The quality of the FEM is directly dependent on the ability of the selected constitutive model to realistically simulate the nonlinear behavior of the soil within the slope [2]. The finite element program used in the slope analysis software is (Slide V6.003). It is a 2-dimensional elasto-plastic finite element program for calculating stresses and displacements around underground openings, and can be used to solve a wide range of slope stability and civil engineering problems. There are two analysis types in the (Slide V6.003); Plane-Strain and Axi-symmetric analyses. Most cases will be simulated using Plane-Strain conditions. The Axi-symmetric option allows analyzing 3-dimensional problems which is rotationally symmetric about an axis. The input is 2-dimensional, but because of the rotational symmetry, but in fact it is a symmetric 3-dimensional problems revolving about an axis (Slide V6.003). The program supports analysis of elastic and plastic materials but plastic material properties are defined only with isotropic properties. The program allows for simulating the construction sequence process by analyzing the model in stages for each construction step. Problem

boundaries, materials properties, support properties, ground water table, loads and other features in the program could also vary in the different stages. The program allows defining soil strength with many strength criteria; Mohr-Coulomb, Hoek-Brown, Generalized Hoek-Brown, Drucker-Prager, Cam-clay, and Modified Cam-Clay [3].

**5 PARAMETRIC STUDY**

This section is concerned in presenting all the parameters used in this research which affect the slope stability, including the geofoam material on the slope safety factor. The soil properties used in the slope analysis is correlated from the soil investigation reports, along with the data presented in Al-Ashaal, (1998). Also, material characteristics are summarized in Tables (2-3). Also, surcharge pressure is applied to simulate a load equivalent to the 70-ton truck, in addition to 0.10 t/m<sup>2</sup> to account for the pavement thickness, with a total test pressure of 3.40 t/m<sup>2</sup>.

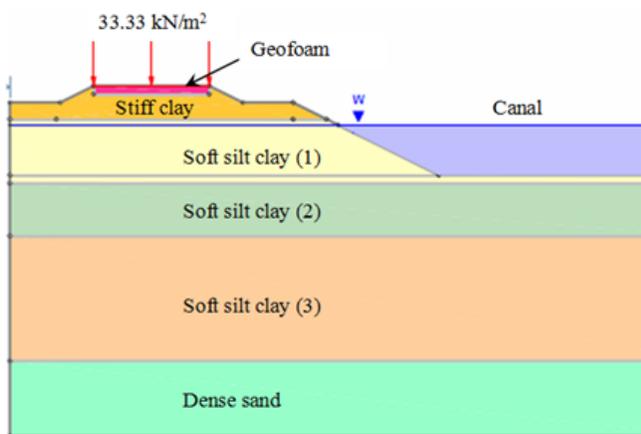
**TABLE 2. THE DEPENDANT SOIL PROPERTIES ON THE SHEAR STRENGTH PARAMETERS. [9]**

Soil Type	$\gamma_{sat}$ (kN/m <sup>3</sup> )	E (MPa)	$\nu$	c (kPa)	$\phi$ (°)	$\psi$ (°)
Soft Silty Clay (1)	17	7	0.45	0	16.	5
Soft Silty Clay (2)	16	4	0.45	0	14.	0
Soft Silty Clay (3)	17	0	0.45	0	23.	0
Stiff Clay layer	17	9	0.45	0	45.	0
Peat layer	11	3	0.45	3.0	0	0
Dense sand	18	10	0.30	0.0	38	8
Gravel layer	19	20	0.30	0.0	45	15

In which:

- $\gamma_{sat}$  : Saturated unit weight;
- E: Soil Young's modulus;
- $\nu$ : Poisson's ratio;
- c: Soil cohesion;
- $\Phi$ : Angle of internal friction; and
- $\Psi$ : Dilation angle ( $\phi-30$ ).

**TABLE 3. MODEL VARIABLES USED IN PARAMETRIC STUDY. [9]**

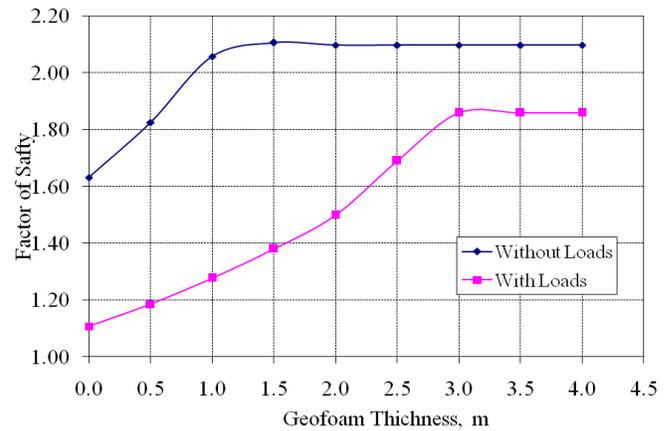


**Fig. 3. Schematic Diagram of the Embankment Showing Soil Stratification**

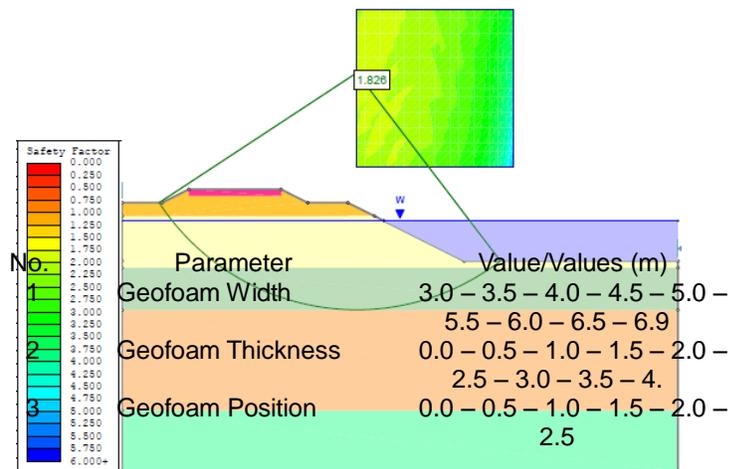
**6 RESULTS**

**6.1. Effect of Geofoam Thickness on Slope stability**

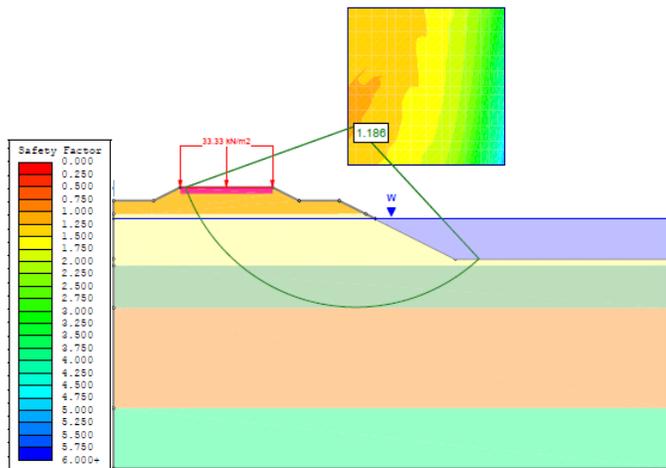
Figure (4) shows the relation between the geofoam thickness (h) and the safety factor of the stabilized slope (F.S.) for geofoam thickness that varies from 0.0m to 4.0m. It is obvious from the figure that increasing the geofoam thickness from 0.0m to 1.0m resulted in a noticeable increase in the safety factor for loaded and unloaded slopes. For unloaded slope, and due to increasing geofoam thickness from 1.0m up to 4.0m, the safety factor is still constant for about 2.10. A consistent increase in the safety factors is noticed as a result of increasing the geofoam thickness from 0.0m up to 4.0m. Figures (5&6) indicate the effect of the geofoam thickness=0.50m on unloaded and loaded slopes, respectively. Geofoam thickness is found to be effective for loaded slopes that because of increasing of the safety factor for about 40%.



**Fig. 4. Effect of Geofoam Thickness on the Factor of Safety**



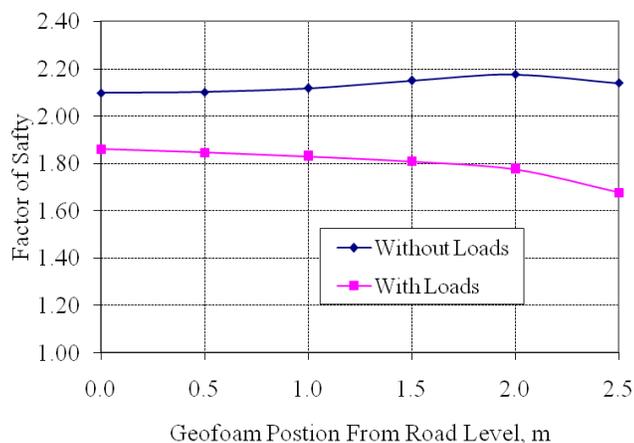
**Fig. 5. Effect of Geofoam Thickness (0.50m) on (F.S.) for Unloaded Slope.**



**Fig. 6.** Effect of Geofabric Thickness (0.50m) on (F.S.) for loaded Slope.

### 6.2. Effect of Geofabric Position from Road Level on Slope stability

Figure (7) shows the effect of varying the depth of geofabric layer from the road level. Positions are varying from 0.0m (at the road level) up to 2.5m from the road level. The geofabric width is constant and equal to embankment width. The studied range of geofabric position (H) from the road level represents a slight increase in the safety factor for unloaded slopes. On the contrary, there is a slight decrease in the safety factor for loaded slopes during different values of geofabric position from the road level.

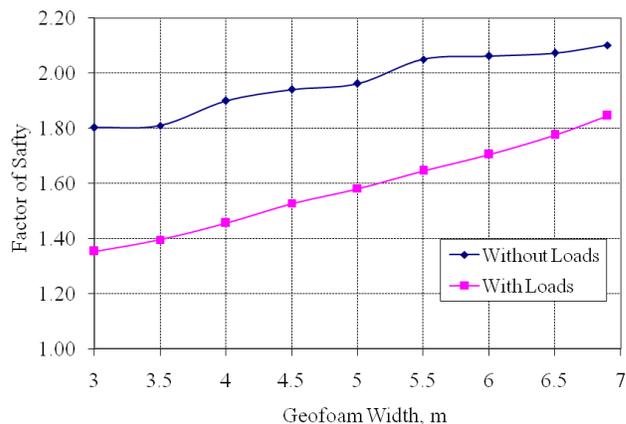


**Fig. 7.** Effect of Geofabric Position from Road Level on the Factor of Safety

### 6.3. Effect of Geofabric Width on Slope stability

Figure (8) shows the relation between the geofabric width (B) and safety factors for constant depth of the geofabric layer of 0.50m from the embankment level. The relation between the geofabric width and safety factors is directly proportional, as increasing the geofabric width will increase the safety factor. For unloaded slopes, there is a slight increase of the safety

factors. The values changed from 1.80 at B = 3m to 2.10 at B = 6.9m. On the other hand, a clear increase is noticed for loaded slopes in safety factors. The values changed from 1.35 at B = 3m to 1.84 at B = 6.9m.



**Fig. 8.** Effect of Geofabric Width on the Factor of Safety

## 7 CONCLUSIONS

This paper presents the results of study of the effect of geofabric on the slope stabilization under loaded and unloaded slope embankment. Based on the results of the current research, the following conclusions are drawn:

- 1- Partial replacement of slope embankment by geofabric is a successful and efficient solution to increase the factor of safety of the slope.
- 2- Limit equilibrium results showed that using a geofabric thickness equal to the 1.0 m is effective in increasing the factor of safety in both loaded and unloaded slope. In addition, the increasing of the safety factor of the loaded slope is about 40%. Thus, it is recommended to use geofabric thickness equal to 1.0 m.
- 3- Results indicated that the position of the geofabric layer from road level is not that effective in reducing the factor of safety. Therefore, a geofabric layer at the road surface with coated by 0.50 m of sand layer is considered efficient and economic.
- 4- Results showed that using a geofabric width for case of loaded and unloaded slope is effective in increasing the factor of safety. The increasing of the safety factor of the unloaded and loaded slope are 34% and 38% respectively.

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